

# Low Noise, Precision CMOS Amplifier

# AD8655

#### **FEATURES**

**Low noise: 2.7 nV/**√**Hz @ f = 10 kHz Low offset voltage: 250 µV max over V**<sup>B</sup> **CM**<sup>B</sup> **Offset voltage drift: 0.4 µV/°C typ and 2.3 µV/°C max Bandwidth: 28 MHz Rail-to-rail input/output Unity gain stable 2.7 V to 5.5 V operation −40°C to +125°C operation** 

#### **APPLICATIONS**

**ADC and DAC buffers Audio Industrial controls Precision filters Digital scales Strain gauges PLL filters** 

#### **GENERAL DESCRIPTION**

The AD8655 is the industry's lowest noise, precision CMOS amplifier. It leverages the Analog Devices DigiTrim® technology to achieve high dc accuracy.

The AD8655 provides low noise (2.7 nV/ $\sqrt{Hz}$  @ 10 kHz), low THD + N (0.0007%), and high precision performance (250  $\mu$ V max over  $V_{CM}$ ) to low voltage applications. The ability to swing rail-to-rail at the input and output enables designers to buffer ADCs and other wide dynamic range devices in single-supply systems.

#### **PIN CONFIGURATIONS**



Figure 2. 8-Lead SOIC (R-8)

**NC = NO CONNECT**

The AD8655 high precision performance improves the resolution and dynamic range in low voltage applications. Audio applications, such as microphone pre-amps and audio mixing consoles, benefit from the low noise, low distortion, and high output current capability of the AD8655 to reduce system level noise performance and maintain audio fidelity. The AD8655's high precision and rail-to-rail input and output benefit data acquisition, process controls, and PLL filter applications.

The AD8655 is fully specified over the −40°C to +125°C temperature range. The AD8655 is available in 8-lead MSOP and SOIC packages.

#### **Rev. 0**

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### **REVISION HISTORY**

4/05-Revision 0: Initial Version

## <span id="page-2-0"></span>5.0 V ELECTRICAL SPECIFICATIONS

 $V_s = 5.0$  V,  $V_{\text{CM}} = V_s/2$ ,  $T_A = 25^{\circ}\text{C}$ , unless otherwise specified.

#### **Table 1.**



## <span id="page-3-0"></span>2.7 V ELECTRICAL SPECIFICATIONS

 $V_s = 2.7$  V,  $V_{\text{CM}} = V_s/2$ ,  $T_A = 25^{\circ}\text{C}$ , unless otherwise specified.

#### **Table 2.**



### <span id="page-4-0"></span>ABSOLUTE MAXIMUM RATINGS

#### **Table 3.**



Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### **Table 4.**



<sup>1</sup>θ<sub>JA</sub> is specified for worst-case conditions, that is, θ<sub>JA</sub> is specified for a device soldered in the circuit board for surface-mount packages.

#### **ESD CAUTION**

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.



## <span id="page-5-0"></span>TYPICAL PERFORMANCE CHARACTERISTICS



Figure 3. Input Offset Voltage Distribution



Figure 4. Input Offset Voltage vs. Temperature



Figure 5.  $|TCV_{OS}|$  Distribution



Figure 6. Input Offset Voltage vs. Common-Mode Voltage



Figure 7. Input Bias Current vs. Temperature



Figure 8. Supply Current vs. Supply Voltage











Figure 11. Output Voltage Swing High vs. Temperature



Figure 12. Output Voltage Swing Low vs. Temperature







Figure 14. Large Signal CMRR vs. Temperature







Figure 16. Large Signal PSSR vs. Temperature



Figure 17. Voltage Noise Density vs. Frequency



Figure 18. Low Frequency Noise (0.1 Hz to 10 Hz ).







Figure 20. Open-Loop Gain and Phase vs. Frequency



Figure 21. Large Signal Open-Loop Gain vs. Temperature







Figure 23. Maximum Output Swing vs. Frequency



Figure 24. Large Signal Response



**TIME (1**µ**s/DIV)**









Figure 27. Negative Overload Recovery Time



Figure 28. Positive Overload Recovery Time



Figure 29. Output Impedance vs. Frequency











Figure 32.  $|TCV_{OS}|$  Distribution











Figure 35. Output Voltage Swing High vs. Temperature



Figure 36. Output Voltage Swing Low vs. Temperature



Figure 37. No Phase Reversal



Figure 38. Large Signal Response



Figure 39. Small Signal Response



Figure 40. Small Signal Overshoot vs. Load Capacitance



Figure 41. Negative Overload Recovery Time



Figure 42. Positive Overload Recovery Time







Figure 44. Large Signal CMRR vs. Temperature









Figure 47. Large Signal Open-Loop Gain vs. Temperature



Figure 48. Closed-Loop Gain vs. Frequency







Figure 50. Output Impedance vs. Frequency

## <span id="page-13-0"></span>THEORY OF OPERATION

The AD8655 amplifier is a voltage feedback, rail-to-rail input and output precision CMOS amplifier, which operates from 2.7 V to 5.0 V of power supply voltage. This amplifier uses the Analog Devices DigiTrim technology to achieve a higher degree of precision than is available from most CMOS amplifiers. DigiTrim technology, used in a number of ADI amplifiers, is a method of trimming the offset voltage of the amplifier after it is packaged. The advantage of post-package trimming is that it corrects any offset voltages caused by the mechanical stresses of assembly.

The AD8655 is available in a standard op amp pinout, making DigiTrim completely transparent to the user. The input stage of the amplifier is a true rail-to-rail architecture, allowing the input common-mode voltage range of the amplifier to extend to both positive and negative supply rails. The open-loop gain of the AD8655 with a load of 10 kΩ is typically 110 dB.

The AD8655 can be used in any precision op amp application. The amplifier does not exhibit phase reversal for common-mode voltages within the power supply. The AD8655 is a great choice for high resolution data acquisition systems with voltage noise of 2.7 nV/ $\sqrt{Hz}$  and THD + Noise of –103 dB for a 2 V p-p signal at 10 kHz. Its low noise, sub-pA input bias current, precision offset, and high speed make it a superb preamp for fast filter applications. The speed and output drive capability of the AD8655 also make it useful in video applications.

### <span id="page-14-0"></span>APPLICATIONS **INPUT OVERVOLTAGE PROTECTION**

The internal protective circuitry of the AD8655 allows voltages exceeding the supply to be applied at the input. It is recommended, however, not to apply voltages that exceed the supplies by more than 0.3 V at either input of the amplifier. If a higher input voltage is applied, series resistors should be used to limit the current flowing into the inputs. The input current should be limited to less than 5 mA.

The extremely low input bias current allows the use of larger resistors, which allows the user to apply higher voltages at the inputs. The use of these resistors adds thermal noise, which contributes to the overall output voltage noise of the amplifier. For example, a 10 k $\Omega$  resistor has less than 12.6 nV/ $\sqrt{Hz}$  of thermal noise and less than 10 nV of error voltage at room temperature.

### **INPUT CAPACITANCE**

Along with bypassing and ground, high speed amplifiers can be sensitive to parasitic capacitance between the inputs and ground. For circuits with resistive feedback network, the total capacitance, whether it is the source capacitance, stray capacitance on the input pin, or the input capacitance of the amplifier causes a breakpoint in the noise gain of the circuit. As a result, a capacitor must be added in parallel with the gain resistor to obtain stability. The noise gain is a function of frequency and peaks at the higher frequencies, assuming the feedback capacitor is selected to make the second-order system critically damped. A few picofarads of capacitance at the input reduce the input impedance at high frequencies, which increases the amplifier's gain, causing peaking in the frequency response or oscillations. With the AD8655, additional input damping is required for stability with capacitive loads greater than 200 pF with direct input to output feedback. See the next section on [Driving Capacitive Loads.](#page-14-1)

#### <span id="page-14-1"></span>**DRIVING CAPACITIVE LOADS**

Although the AD8655 can drive capacitive loads up to 500 pF without oscillating, a large amount of ringing is present when operating the part with input frequencies above 100 kHz. This is especially true when the amplifier is configured in positive unity gain (worst case). When such large capacitive loads are required, the use of external compensation is highly recommended. This reduces the overshoot and minimizes ringing, which in turn, improves the stability of the AD8655 when driving large capacitive loads.

One simple technique for compensation is a snubber that consists of a simple RC network. With this circuit in place, output swing is maintained, and the amplifier is stable at all gains. [Figure 52 s](#page-14-2)hows the implementation of a snubber, which reduces overshoot by more than 30% and eliminates ringing. Using a snubber does not recover the loss of bandwidth incurred from a heavy capacitive load.



Figure 51. Driving Heavy Capacitive Loads Without Compensation

<span id="page-14-2"></span>





Figure 53. Driving Heavy Capacitive Loads Using a Snubber Network

#### **THD Readings vs. Common-Mode Voltage**

Total harmonic distortion of the AD8655 is well below 0.0007% with a load of 1 k $\Omega$ . The distortion is a function of the circuit configuration, the voltage applied, and the layout, in addition to other factors.



Figure 54. THD + N Test Circuit



Figure 55. THD + Noise vs. Frequency

### <span id="page-16-0"></span>LAYOUT, GROUNDING, AND BYPASSING CONSIDERATIONS **POWER SUPPLY BYPASSING**

Power supply pins can act as inputs for noise, so care must be taken to apply a noise-free, stable dc voltage. The purpose of bypass capacitors is to create low impedances from the supply to ground at all frequencies, thereby shunting or filtering most of the noise. Bypassing schemes are designed to minimize the supply impedance at all frequencies with a parallel combination of capacitors with values of 0.1 µF and 4.7 µF. Chip capacitors of  $0.1 \mu$ F (X7R or NPO) are critical and should be as close as possible to the amplifier package. The 4.7 µF tantalum capacitor is less critical for high frequency bypassing, and, in most cases, only one is needed per board at the supply inputs.

#### **GROUNDING**

A ground plane layer is important for densely packed PC boards to minimize parasitic inductances. This minimizes voltage drops with changes in current. However, an understanding of where the current flows in a circuit is critical to implementing effective high speed circuit design. The length of the current path is directly proportional to the magnitude of parasitic inductances, and, therefore, the high frequency impedance of the path. Large changes in currents in an inductive ground return create unwanted voltage noise.

The length of the high frequency bypass capacitor leads is critical, and, therefore, surface-mount capacitors are recommended. A parasitic inductance in the bypass ground trace works against the low impedance created by the bypass capacitor. Because load currents flow from the supplies, the ground for the load impedance should be at the same physical location as the bypass capacitor grounds. For larger value capacitors intended to be effective at lower frequencies, the current return path distance is less critical.

### **LEAKAGE CURRENTS**

Poor PC board layout, contaminants, and the board insulator material can create leakage currents that are much larger than the input bias current of the AD8655. Any voltage differential between the inputs and nearby traces sets up leakage currents through the PC board insulator, for example,  $1 \text{ V}/100 \text{ G}\Omega$  = 10 pA. Similarly, any contaminants on the board can create significant leakage (skin oils are a common problem).

To significantly reduce leakage, put a guard ring (shield) around the inputs and input leads that are driven to the same voltage potential as the inputs. This ensures that there is no voltage potential between the inputs and the surrounding area to set up any leakage currents. To be effective, the guard ring must be driven by a relatively low impedance source and should completely surround the input leads on all sides, above and below, by using a multilayer board.

The charge absorption of the insulator material itself can also cause leakage currents. Minimizing the amount of material between the input leads and the guard ring helps to reduce the absorption. Also, low absorption materials, such as Teflon® or ceramic, may be necessary in some instances.

## <span id="page-17-0"></span>OUTLINE DIMENSIONS



Figure 56. 8-Lead Standard Small Outline Package [SOIC] Narrow Body (R-8)

Dimensions shown in millimeters and (inches)



(RM-8) Dimensions shown in millimeters

#### **ORDERING GUIDE**

<span id="page-17-1"></span>

<span id="page-17-2"></span> $1 Z = Pb$ -free part.

## **NOTES**

**NOTES** 



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